



FC488-90B-FC - JUN 03, 2021

Item # FC488-90B-FC was discontinued on JUN 03, 2021. For informational purposes, this is a copy of the website content at that time and is valid only for the stated product.

488 NM SINGLE MODE FUSED FIBER OPTIC COUPLERS / TAPS





Insertion Loss_{port1→port3}(
$$dB$$
) = 10 log $\frac{P_{port1}(mW)}{P_{port3}(mW)}$

Insertion Loss_{port1→port4}(
$$dB$$
) = 10 log $\frac{P_{port1}(mW)}{P_{port4}(mW)}$

A similar equation can be used to define the insertion loss at port 2 for input at port 1. However, as seen above, this is already defined as the directivity of the coupler.

Insertion loss inherently includes both coupling (e.g., light transferred to the other output leg) and excess loss (e.g., light lost from the coupler) effects. The maximum allowed insertion loss for each output, signal and tap, are both specified. Because the insertion loss in each output is correlated to light coupled to the other output, no coupler will ever have the maximum insertion loss in both outputs simultaneously.

Calculating Insertion Loss using Power Expressed in dBm

Insertion loss can also be easily calculated with the power expressed in units of dBm. The equation below shows the relationship between power expressed in mW and dBm:

$$P(dBm) = 10 \log P(mW)$$

Then, the insertion loss in dB can be calculated as follows:

Insertion Loss
$$(dB) = P_{in}(dBm) - P_{out}(dBm)$$

Coupling Ratio

Insertion loss (in dB) is the ratio of the input power to the output power from each leg of the coupler as a function of wavelength. It captures both the coupling ratio and the excess loss. The coupling ratio is calculated from the measured insertion loss. Coupling ratio (in %) is the ratio of the optical power from each output port (A and B) to the sum of the total power of both output ports as a function of wavelength. It is not impacted by spectral features such as the water absorption region because both output legs are affected equally.





Uniformity

The uniformity is also calculated from the measured insertion loss. Uniformity is the variation (in dB) of the insertion loss over the bandwidth. It is a measure of how evenly the insertion loss is distributed over the spectral range. The uniformity of Path A is the difference between the value of highest insertion loss and the solid red insertion loss curve (in the Insertion Plot above). The uniformity of Path B is the difference between the solid blue insertion loss curve and the value of lowest insertion loss.



A graphical representation of the Uniformity calculation.

General Coupling Examples

Animated example of 90:10 splitting and 50:50 mixing.

2x2 fused fiber optic couplers can split or mix light between two optical fibers with minimal loss and at a specified coupling ratio. Thorlabs' couplers are available from stock in one of four ratios: 50:50, 75:25, 90:10, or 99:1. All of our fused fiber optic couplers are bidirectional, meaning that all ports can be used as an input. The animation to the right shows several simple coupling examples.

The terms "Signal Output" and "Tap Output" refer to the higher and lower power outputs, respectively. To illustrate this, if light is input into the white port of the TW1064R1A2A coupler (99:1 coupling ratio), 99% of the transmitted light is coupled into the white port on the other side of the coupler while the other 1% is coupled into the red port. In this example, the second white port is referred to as the signal output port, and the red port is referred to as a tap output port. For a 50:50 coupler, the signal and tap ports would have the same power output.

In our couplers with a red housing, the signal always propagates from blue to red or white to white, while the tap always propagates from blue to white or white to red. For other couplers, please refer to the datasheet included with the coupler to determine signal and tap propagation paths.

Specific Coupling Examples

In the examples below, two 2x2 1300 nm Wideband Fiber Optic Couplers (50:50 and 90:10 coupling ratios) are used with input signals A and B. The table to the right lists typical insertion loss (signal and tap outputs) for each coupler. To calculate the power at any given output, subtract the insertion loss for the signal or tap output from the input power (in dBm).

Coupling Ratio	Insertion Loss (Signal)	Insertion Loss (Tap)
90:10	0.6 dB	10.1 dB
50:50	3.2 dB	3.2 dB

Example 1: Splitting Light from a Single Input

For this example, the couplers are used to split light from a single input into the signal and tap outputs as indicated in the diagrams below. In the table below, the output ports are highlighted in green.

	90:10 Coupling Ratio	50:50 Coupling Ratio
Port	Signal A	Signal A
1 (Input)	10 dBm (10 mW)	10 dBm (10 mW)
2 (Not Used)	-	-
3 (Tap Output)	-0.1 dBm (1.0 mW)	6.8 dBm (4.8 mW)
4 (Signal Output)	9.4 dBm (8.7 mW)	6.8 dBm (4.8 mW)
Click on the Diagram for Power Distributions at Each Port	Port 4: Output A (Signal) 90:10 Coupling Ratio Port 1: Input A Port 3: Output A (Tap)	Port 4: Outp

Example 2: Mixing Two Signals from Two Inputs

In this example, the couplers are used to mix light from two inputs, designated Signal A and Signal B. The outputs contain a mixed signal composed of both Signal A and Signal B in ratios depending on the coupling ratio. All ports are indicated in the diagrams below. In the table below, the output ports are highlighted in green.

				l	
	90:10 Co	upling Ratio	50:50 Coupling Ratio		
Port	Signal A	Signal B	Signal A	Sig	
1 (Input A)	5 dBm (3.2 mW)	-	5 dBm (3.2 mW)		
2 (Input B)	-	8 dBm (6.3 mW)	-	8 dBm	
3 (Output)	-5.1 dBm (0.3 mW)	7.4 dBm (5.5 mW)	1.6 dBm (1.4 mW)	4.8 dBm	
4 (Output)	4.4 dBm (2.8 mW)	-2.1 dBm (0.6 mW)	1.6 dBm (1.4 mW)	4.8 dBm	
	Port 2: Input B	Port 4: Output A (Signal) Output B (Tap)	Port 2: Input B	Port 4: 0u	
Click on the Diagram for Power Distributions at Each Port	90:10 Co	upling Ratio		0 Coupling Ratio	
	Port 1: Input A	Port 3: Output A (Tap) Output B (Signal)	Port 1: Input A	Port 3: (Out	

Example 3: Coupling a Return Signal with a Reflector on Port 3

Here, the couplers are used to split light from a single input, however, in this example there is a 100% reflector on port 3, as shown in the diagrams below. As a result, the light is reflected back into the coupler and split again. The ports are indicated in the diagrams below. In the table below, the output ports for the initial pass are highlighted in green.

	90:10 Coupling R	50:50 Coupling Ra	atio		
Port	Signal A	Signal A Reflected Signal A Signal A			
1 (Input)	6 dBm (4.0 mW)	-14.2 dBm (0.04 mW)	6 dBm (4.0 mW)		
2 (No Input)	-	-4.7 dBm (0.34 mW)	-		
3 (Reflected Output)	-4.1 dBm (0.39 mW) Reflected	-	2.8 dBm (1.9 mW) Reflected		
4 (Signal Output)	5.4 dBm (3.5 mW)	- 2.8 dBm (1.9 mW)			



COUPLER VERIFICATION

Wideband Fiber Coupler Testing and Verification Procedure

During Thorlabs' coupling manufacturing process, the coupling ratio and bandwidth of each wideband coupler is monitored as the two branches are fused together. This ensures that each coupler meets the stated specifications over the bandwidth. Each wideband coupler is shipped with an individualized data sheet providing a summary of the results of these tests. Click here for a sample data sheet for our 470 nm wideband couplers.

Step 1

The fiber to create the first branch (Path A) of the coupler is connected to a source on one side and a switch leading to an Optical Spectrum Analyzer (OSA) on the other.

Step 2

The spectrum of the source through the fiber and switch is measured using the OSA and zeroed.



Click to Enlarge



The fiber to form the second branch (Path B) of the coupler is connected to the source and to the second port of the switch leading to the OSA. The spectrum of the source through the fiber and switch is also measured and zeroed.

Step 4

The two fibers are fused on a manufacturing station to create the coupler structure. During the fusing process, the output from both legs of the coupler is monitored on the OSA. Coupler fusing stops once the coupler reaches the desired coupling ratio, excess loss, and insertion loss specifications.



Click to Enlarge

For 1x2 couplers, one of the fiber ends is terminated within the coupler housing. The termination is done in a manner that minimizes back reflections from this output.



Insertion loss (in dB) is the ratio of the input power to the output power from each leg of the coupler as a function of wavelength. It captures both the coupling ratio and the excess loss. The coupling ratio is calculated from the measured insertion loss. Coupling ratio (in %) is the ratio of the optical power from each output port (A and B) to the sum of the total power of both output ports as a function of wavelength. It is not impacted by spectral features such as the water absorption region because both output legs are affected equally. Persistence plots showing the coupling ratio of our wideband couplers can be viewed by clicking on the blue info icons below.



The uniformity is also calculated from the measured insertion loss. Uniformity is the variation (in dB) of the insertion loss over the bandwidth. It is a measure of how evenly the insertion loss is distributed over the spectral range. The uniformity of Path A is the difference between the value of highest insertion loss and the solid red insertion loss curve (in the Insertion Plot above). The uniformity of Path B is the difference between the solid blue insertion loss curve and the value of lowest insertion loss. Persistence plots showing the uniformity of our wideband couplers can be viewed by clicking on the blue info icons below.

	• •	
RELIABILITY TESTING		
GR-1221-CORE Testing	Requirement Limits	
Our 2x2 1300 nm Single Mode Fused Fiber Optic Couplers have undergone a reliability testing program inspired by GR-1221-CORE (Generic Reliability Assurance Requirements for Passive Optical Components, Issue 2). The selecter	Parameter	Limit
test conditions are for uncontrolled environments and are some of the most stringent test conditions for passive components. The results of this testing program qualify these couplers and their manufacturing process for volume	Change in Insertion Loss (ΔIL)	≤0.2 dB
production and use in uncontrolled environments. To download a PDF of this test report, please click here.	Coupling Ratio	±1.5%
Enlarge Click To Enlarge		

Close-Up of Mechanical Shock Test Setup



SM-105 Mechanical Shock Test Machine



Click To Enlarge

Damp Heat Testing Setup

Testing Conditions

This test program consisted of five test groups with a sample size of 11 per group. Testing was conducted with a 1310 nm laser source input into 1310 tap couplers using a 1x16 waveguide coupler. The two outputs of every coupler were measured by a PM100USB power meter with an S154C sensor head.

	Testing Conditions	
Mechanical Testing (Group 1)		
Environmental and Mechanical Testing Laborato mechanical shock using an Avex SM-105 mecha	derwent three mechanical tests; the mechanical shock and vibration ny while the fiber side pull tests were performed in-house. In one test anical shock test machine with a 3200B4 accelerometer. In another, t ration system with a VT1436 vibration controller and a 356A01 accel a weight of 0.23 kg at 90° for 5 seconds.	t, the couplers were induced wit hey were induced with vibratior
Test Parameter	Conditions	Reference
Mechanical Shock	Acceleration: 500 g Pulse Width: 1 ms Pulse Shape: Half-Sine # of Directions: 6 # of Shocks/Direction: 5	MIL-STD-993 Method 2002
Vibration	Acceleration: 20 g Frequency Range: 20 Hz to 2000 Hz Duration: 4 min/cycle Number of Cycles/Axis: 4 Axes: X, Y, Z	MIL-STD-883 Method 2007 Condition A
Fiber Side Pull	0.23 kg, 90°, 5 sec, 2 directions	GR-1209-CORE
		Click for Graphs: More [+
Damp Heat Storage (Group 2)		
The performance of these couplers was tested in maintain an 85 $^{\circ}$ C ± 2 $^{\circ}$ C temperature with 85%	n damp heat at a Thorlabs facility. A Test Equity Model 115A Tempera ± 5% relative humidity for 2000 hours.	ature Chamber was used to
Test Parameter	Conditions	Reference
Damp Heat	85 °C (±2 °C) 85% (±5%) Relative Humidity 2000 Hours	MIL-STD-883 Method 103
	I	Click for Graphs: More [+
High Temperature Storage (Group 3)		
The performance of these couplers was tested in used to maintain an 85 °C ± 2 °C temperature w	n dry high temperatures in a Thorlabs facility. A Test Equity Model 11: ith <40% Relative Humidity for 2000 hours.	5A Temperature Chamber was
Test Parameter	Conditions	Reference
High Temperature Storage (Dry Heat)	85 °C (±2 °C) <40% Relative Humidity 2000 Hours	EIA/TIA-455-4A
		Click for Graphs: More [+
Low Temperature Storage (Group 4)		
The performance of these couplers was tested in to maintain a -40 °C ± 5 °C temperature with uno	n low temperatures at a Thorlabs facility. A Test Equity Model 115A Tr controlled relative humidity for 2000 hours.	emperature Chamber was used
Test Parameter	Conditions	Reference
Low Temperature Storage	-40 °C (±5 °C) Uncontrolled Relative Humidity 2000 Hours	EIA/TIA-455-4A

Testing Conditions Temperature Cycling (Group 5)							
Temperature Cycling (Group 5)							
21 I	of these couplers was tested during temperature cycling of their environment. with a 10 minutes pause at room temperature at each cycle.	The temperature varied from -40					
Test Parameter	Conditions	Reference					
The second se	-40 °C to 85 °C (±2 °C)	MIL-STD-883					
Temperature Cycling	400 Cycles with 10 Minute Pause at Room Temperature	Method 1010					
		Click for Graphs: More [+]					

Laser-Induced Damage in Silica Optical Fibers

The following tutorial details damage mechanisms relevant to unterminated (bare) fiber, terminated optical fiber, and other fiber components from laser light sources. These mechanisms include damage that occurs at the air / glass interface (when free-space coupling or when using connectors) and in the optical fiber itself. A fiber component, such as a bare fiber, patch cable, or fused coupler, may have multiple potential avenues for damage (e.g., connectors, fiber

Quick Links
Damage at the Air / Glass Interface
Intrinsic Damage Threshold
Preparation and Handling of Optical Fibers

end faces, and the device itself). The maximum power that a fiber can handle will always be limited by the lowest limit of any of these damage mechanisms.

While the damage threshold can be estimated using scaling relations and general rules, absolute damage thresholds in optical fibers are very application dependent and user specific. Users can use this guide to estimate a safe power level that minimizes the risk of damage. Following all appropriate preparation and handling guidelines, users should be able to operate a fiber component up to the specified maximum power level; if no maximum is specified for a component, users should abide by the "practical safe level" described below for safe operation of the component. Factors that can reduce power handling and cause damage to a fiber component include, but are not limited to, misalignment during fiber coupling, contamination of the fiber end face, or imperfections in the fiber itself. For further discussion about an optical fiber's power handling abilities for a specific application, please contact Thorlabs' Tech Support.

Damage at the Air / Glass Interface

There are several potential damage mechanisms that can occur at the air / glass interface. Light is incident on this interface when free-space coupling or when two fibers are mated using optical connectors. High-intensity light can damage the end face leading to reduced power handling and permanent damage to the fiber. For fibers terminated with optical connectors where the connectors are fixed to the fiber ends using epoxy, the heat generated by high-intensity light can burn the epoxy and leave residues on the fiber facet directly in the beam path.



Click to Enlarge Undamaged Fiber End

Damage Mechanisms on the Bare Fiber End Face

Damage mechanisms on a fiber end face can be modeled similarly to bulk optics, and industry-standard damage thresholds for UV Fused Silica substrates can be applied to silica-based fiber. However, unlike bulk optics, the relevant surface areas and beam diameters involved at the air / glass interface of an optical fiber are very small, particularly for coupling into single mode (SM) fiber. therefore, for a given power density, the power incident on the fiber needs to be lower for a smaller beam diameter.

The table to the right lists two thresholds for optical power densities: a theoretical damage threshold and a "practical safe level". In general, the theoretical damage threshold represents the estimated maximum power density that can be incident on the fiber end face without risking damage with very good fiber end face and coupling conditions. The "practical safe level" power density represents minimal risk of fiber damage. Operating a fiber or component beyond the practical safe level is possible, but users must follow the appropriate handling instructions and verify performance at low powers prior to use.

Estimated	Optical Power Densities on A	Air / Glass Interface ^a
Туре	Theoretical Damage Threshold ^b	Practical Safe Level ^c
CW (Average Power)	~1 MW/cm ²	~250 kW/cm ²
10 ns Pulsed (Peak Power)	~5 GW/cm ²	~1 GW/cm ²

- All values are specified for unterminated (bare) silica fiber and apply for free space coupling into a clean fiber end face.
- This is an estimated maximum power density that can be incident on a fiber end face without risking damage. Verification of the performance and reliability of fiber components in the system before operating at high power must be done by the user, as it is highly system dependent.
- This is the estimated safe optical power density that can be incident on a fiber end face without damaging the fiber under most operating conditions.

Calculating the Effective Area for Single Mode and Multimode Fibers

The effective area for single mode (SM) fiber is defined by the mode field diameter (MFD), which is the cross-sectional area through which light propagates in the fiber; this area includes the fiber core and also a portion of the cladding. To achieve good efficiency when coupling into a single mode fiber, the diameter of the input beam must match the MFD of the fiber.

As an example, SM400 single mode fiber has a mode field diameter (MFD) of ~Ø3 µm operating at 400 nm, while the MFD for SMF-28 Ultra single mode fiber operating at 1550 nm is Ø10.5 µm. The effective area for these fibers can be calculated as follows:

SM400 Fiber: Area = Pi x $(MFD/2)^2$ = Pi x $(1.5 \ \mu m)^2$ = 7.07 μm^2 = 7.07 x $10^{-8} \ cm^2$

SMF-28 Ultra Fiber: Area = Pi x $(MFD/2)^2$ = Pi x $(5.25 \ \mu m)^2$ = 86.6 μm^2 = 8.66 x $10^{-7} \ cm^2$

To estimate the power level that a fiber facet can handle, the power density is multiplied by the effective area. Please note that this calculation assumes a uniform intensity profile, but most laser beams exhibit a Gaussian-like shape within single mode fiber, resulting in a higher power density at the center of the beam compared to the edges. Therefore, these calculations will slightly overestimate the power corresponding to the damage threshold or the practical safe level. Using the estimated power densities assuming a CW light source, we can determine the corresponding power levels as:

SM400 Fiber: 7.07 x 10⁻⁸ cm² x 1 MW/cm² = 7.1 x 10⁻⁸ MW = 71 mW (Theoretical Damage Threshold) 7.07 x 10⁻⁸ cm² x 250 kW/cm² = 1.8 x 10⁻⁵ kW = 18 mW (Practical Safe Level)

SMF-28 Ultra Fiber: 8.66 x 10⁻⁷ cm² x 1 MW/cm² = 8.7 x 10⁻⁷ MW = 870 mW (Theoretical Damage Threshold) 8.66 x 10⁻⁷ cm² x 250 kW/cm² = 2.1 x 10⁻⁴ kW = 210 mW (Practical Safe Level)

The effective area of a multimode (MM) fiber is defined by the core diameter, which is typically far larger than the MFD of an SM fiber. For optimal coupling, Thorlabs recommends focusing a beam to a spot roughly 70 - 80% of the core diameter. The larger effective area of MM fibers lowers the power density on the fiber end face, allowing higher optical powers (typically on the order of kilowatts) to be coupled into multimode fiber without damage.

Damage Mechanisms Related to Ferrule / Connector Termination

Fibers terminated with optical connectors have additional power handling considerations. Fiber is typically terminated using epoxy to bond the fiber to a ceramic or steel ferrule. When light is coupled into the fiber through a connector, light that does not enter the core and propagate down the fiber is scattered into the outer layers of the fiber, into the ferrule, and the epoxy used to hold the fiber in the ferrule. If the light is intense enough, it can burn the epoxy, causing it to vaporize and deposit a residue on the face of the connector. This results in localized absorption sites on the fiber end face that reduce coupling efficiency and increase scattering, causing further damage.

For several reasons, epoxy-related damage is dependent on the wavelength. In general, light scatters more strongly at short wavelengths than at longer wavelengths. Misalignment when coupling is also more likely due to the small MFD of short-wavelength SM fiber that also produces more scattered light.

To minimize the risk of burning the epoxy, fiber connectors can be constructed to have an epoxyfree air gap between the optical fiber and ferrule near the fiber end face. Our high-power multimode fiber patch cables use connectors with this design feature.

Determining Power Handling with Multiple Damage Mechanisms



When fiber cables or components have multiple avenues for damage (e.g., fiber patch cables), the maximum power handling is always limited by the lowest damage threshold that is relevant to the fiber component. In general, this represents the highest input power that can be incident on the patch cable end face and not the coupled output power. Plot showing approximate input power that can be incident on a single mode silica optical fiber with a termination. Each line shows the estimated power level due to a specific damage mechanism. The maximum power handling is limited by the lowest power level from all relevant damage mechanisms (indicated by a solid line).

As an illustrative example, the graph to the right shows an estimate of the power handling limitations of a single mode fiber patch cable due to damage to the fiber end face and damage via an optical connector. The total input power handling of a terminated fiber at a given wavelength is limited by the lower of the two limitations at any given wavelength (indicated by the solid lines). A single mode fiber operating at around 488 nm is primarily limited by damage to the fiber end face (blue solid line), but fibers operating at 1550 nm are limited by damage to the optical connector (red solid line).

In the case of a multimode fiber, the effective mode area is defined by the core diameter, which is larger than the effective mode area for SM fiber. This results in a lower power density on the fiber end face and allows higher optical powers (on the order of kilowatts) to be coupled into the fiber without damage (not shown in graph). However, the damage limit of the ferrule / connector termination remains unchanged and as a result, the maximum power handling for a multimode fiber is limited by the ferrule and connector termination.

Please note that these are rough estimates of power levels where damage is very unlikely with proper handling and alignment procedures. It is worth noting that optical fibers are frequently used at power levels above those described here. However, these applications typically require expert users and testing at lower powers first to minimize risk of damage. Even still, optical fiber components should be considered a consumable lab supply if used at high power levels.

Intrinsic Damage Threshold

In addition to damage mechanisms at the air / glass interface, optical fibers also display power handling limitations due to damage mechanisms within the optical fiber itself. These limitations will affect all fiber components as they are intrinsic to the fiber itself. Two categories of damage within the fiber are damage from bend losses and damage from photodarkening.

Bend Losses

Bend losses occur when a fiber is bent to a point where light traveling in the core is incident on the core/cladding interface at an angle higher than the critical angle, making total internal reflection impossible. Under these circumstances, light escapes the fiber, often in a localized area. The light escaping the fiber typically has a high power density, which burns the fiber coating as well as any surrounding furcation tubing.

A special category of optical fiber, called double-clad fiber, can reduce the risk of bend-loss damage by allowing the fiber's cladding (2nd layer) to also function as a waveguide in addition to the core. By making the critical angle of the cladding/coating interface higher than the critical angle of the core/clad interface, light that escapes the core is loosely confined within the cladding. It will then leak out over a distance of centimeters or meters instead of at one localized spot within the fiber, minimizing the risk of damage. Thorlabs manufactures and sells 0.22 NA double-clad multimode fiber, which boasts very high, megawatt range power handling.

Photodarkening

A second damage mechanism, called photodarkening or solarization, can occur in fibers used with ultraviolet or short-wavelength visible light, particularly those with germanium-doped cores. Fibers used at these wavelengths will experience increased attenuation over time. The mechanism that causes photodarkening is largely unknown, but several fiber designs have been developed to mitigate it. For example, fibers with a very low hydroxyl ion (OH) content have been found to resist photodarkening and using other dopants, such as fluorine, can also reduce photodarkening.

Even with the above strategies in place, all fibers eventually experience photodarkening when used with UV or short-wavelength light, and thus, fibers used at these wavelengths should be considered consumables.

Preparation and Handling of Optical Fibers

General Cleaning and Operation Guidelines

These general cleaning and operation guidelines are recommended for all fiber optic products. Users should still follow specific guidelines for an individual product as outlined in the support documentation or manual. Damage threshold calculations only apply when all appropriate cleaning and handling procedures are followed.

- 1. All light sources should be turned off prior to installing or integrating optical fibers (terminated or bare). This ensures that focused beams of light are not incident on fragile parts of the connector or fiber, which can possibly cause damage.
- 2. The power-handling capability of an optical fiber is directly linked to the quality of the fiber/connector end face. Always inspect the fiber end prior to connecting the fiber to an optical system. The fiber end face should be clean and clear of dirt and other contaminants that can cause scattering of coupled light. Bare fiber should be cleaved prior to use and users should inspect the fiber end to ensure a good quality cleave is achieved.
- 3. If an optical fiber is to be spliced into the optical system, users should first verify that the splice is of good quality at a low optical power prior to highpower use. Poor splice quality may increase light scattering at the splice interface, which can be a source of fiber damage.
- 4. Users should use low power when aligning the system and optimizing coupling; this minimizes exposure of other parts of the fiber (other than the core) to light. Damage from scattered light can occur if a high power beam is focused on the cladding, coating, or connector.

Tips for Using Fiber at Higher Optical Power

Optical fibers and fiber components should generally be operated within safe power level limits, but under ideal conditions (very good optical alignment and very clean optical end faces), the power handling of a fiber component may be increased. Users must verify the performance and stability of a fiber component within their system prior to increasing input or output power and follow all necessary safety and operation instructions. The tips below are useful suggestions when considering increasing optical power in an optical fiber or component.

- Splicing a fiber component into a system using a fiber splicer can increase power handling as it minimizes possibility of air/fiber interface damage. Users should follow all appropriate guidelines to prepare and make a high-quality fiber splice. Poor splices can lead to scattering or regions of highly localized heat at the splice interface that can damage the fiber.
- After connecting the fiber or component, the system should be tested and aligned using a light source at low power. The system power can be ramped up slowly to the desired output power while periodically verifying all components are properly aligned and that coupling efficiency is not changing with respect to optical launch power.
- 3. Bend losses that result from sharply bending a fiber can cause light to leak from the fiber in the stressed area. When operating at high power, the localized heating that can occur when a large amount of light escapes a small localized area (the stressed region) can damage the fiber. Avoid disturbing or accidently bending fibers during operation to minimize bend losses.
- 4. Users should always choose the appropriate optical fiber for a given application. For example, large-mode-area fibers are a good alternative to standard single mode fibers in high-power applications as they provide good beam quality with a larger MFD, decreasing the power density on the air/fiber interface.
- Step-index silica single mode fibers are normally not used for ultraviolet light or high-peak-power pulsed applications due to the high spatial power densities associated with these applications.

SM COUPLER GUIDE

Our 1x2 and 2x2 Single Mode Coupler offerings are outlined in the graphs below. Click on the colored bars to visit the web presentation for each coupler. Note that the 1020 nm ± 50 nm (orange bars) option is designed for high power applications up to 50 W.





50:50 Fiber Optic Couplers

Item #	Info	Center Wavelength	Bandwidth	Coupling Ratio ^a (%)	Coupling Ratio Tolerance	Insertion Loss ^a	Excess Loss ^a	Uniformity ^a	Fiber Type ^b	Termina
TW470R5F2 ^{c,d}	0	470 nm	±40 nm	50:50	±6.0%	≤3.9 dB / ≤3.9 dB	≤0.3 dB	≤0.8 dB	460HP	FC/F
TW470R5A2 ^{c,d}	0	4701111	140 1111	(Click for Plot)	10.0%	//9 UD	_⊐0.3 0D	(Click for Plot)	40000	FC/AI

• Please see the 2x2 Coupler Tutorial tab for more information on these terms.

Other fiber types may be available upon request. Please contact Tech Support with inquiries.

• All values are specified at room temperature over the bandwidth and measured without connectors using the white port as the input, as indicated in the diagram above; performance may vary if the blue port is used as the input.

• Below the cut-off wavelength, single mode operation is not guaranteed (click on the blue info icon for more information).

Part Number	Description	Price	Availability
TW470R5F2	2x2 Wideband Fiber Optic Coupler, 470 ± 40 nm, 50:50 Split, FC/PC	\$398.22	Today
TW470R5A2	2x2 Wideband Fiber Optic Coupler, 470 ± 40 nm, 50:50 Split, FC/APC	\$441.50	Today

75:25 Fiber Optic Couplers										
Item #	Info	Center Wavelength	Bandwidth	Coupling Ratio ^a (%)	Coupling Ratio Tolerance	Insertion Loss ^a	Excess Loss ^a	Uniformity ^a	Fiber Type ^b	Termin
TW470R3F2 ^{c,d}	1	470 nm	±40 nm	75:25	±3.75%	≤1.8 dB / ≤7.0 dB	≤0.3 dB	≤1.0 dB	460HP	FC/F
TW470R3A2 ^{c,d}	0	4701111	140 1111	(Click for Plot)	13.7370	1.0 ub / 1.0 ub	20.3 GD	(Click for Plot)	400112	FC/A

• Please see the 2x2 Coupler Tutorial tab for more information on these terms.

Other fiber types may be available upon request. Please contact Tech Support with inquiries.

• All values are specified at room temperature over the bandwidth and measured without connectors using the white port as the input, as indicated in the diagram above; performance may vary if the blue port is used as the input.

• Below the cut-off wavelength, single mode operation is not guaranteed (click on the blue info icon for more information).

Part Number	Description	Price	Availability
TW470R3F2	2x2 Wideband Fiber Optic Coupler, 470 ± 40 nm, 75:25 Split, FC/PC	\$398.22	Today
TW470R3A2	2x2 Wideband Fiber Optic Coupler, 470 ± 40 nm, 75:25 Split, FC/APC	\$441.50	Today

90:10 Fiber Optic Couplers

Item #	Info	Center Wavelength	Bandwidth	Coupling Ratio ^a (%)	Coupling Ratio Tolerance	Insertion Loss ^a	Excess Loss ^a	Uniformity ^a	Fiber Type ^b	Termina
TW470R2F2 ^{c,d} TW470R2A2 ^{c,d}	0	470 nm	±40 nm	90:10 (Click for Plot)	±3.0%	≤0.9 dB / ≤11.8 dB	≤0.3 dB	≤1.0 dB (Click for Plot)	460HP	FC/F FC/A
FC488-90B-FC	0	488 nm	+15 nm	90:10		1.2 dB / 11 dB	1.0 dB		460HP	FC/F
FC488-90B-APC	1	400 1111	101111	30.10	-	(Typical)	(Typical)	-	400111	FC/A

Please see the 2x2 Coupler Tutorial tab for more information on these terms.
 Other fiber types may be available upon request. Please contact Tech Support with inquiries.

All values are specified at room temperature over the bandwidth and measured without connectors using the white port as the input, as indicated in the diagram above; performance may vary if the blue port is used as the input. The FC488-90B-FC and FC488-90B-APC will be retired without replacment when stock is depleted. If you require these parts for line production, please contact Tech Support.

Below the cut-off wavelength, single mode operation is not guaranteed (click on the blue info icon for more information).

Part Number	Description	Price	Availability
TW470R2F2	2x2 Wideband Fiber Optic Coupler, 470 ± 40 nm, 90:10 Split, FC/PC	\$398.22	Today
TW470R2A2	2x2 Wideband Fiber Optic Coupler, 470 ± 40 nm, 90:10 Split, FC/APC	\$441.50	Today
FC488-90B-FC	2x2 Fiber Optic Coupler, 488 ± 15 nm, 90:10 Split, FC/PC	\$248.89	Lead Time
FC488-90B-APC	2x2 Fiber Optic Coupler, 488 ± 15 nm, 90:10 Split, FC/APC	\$293.25	Lead Time

99:1 Fiber Optic Couplers

Item #	Info	Center Wavelength	Bandwidth	Coupling Ratio ^a (%)	Coupling Ratio Tolerance	Insertion Loss ^a	Excess Loss ^a	Uniformity ^a	Fiber Type ^b	Termina
TW470R1F2 ^{c,d}	0	470 nm	±40 nm	99:1	±0.6%	≤0.4 dB / ≤24.3 dB	≤0.3 dB	≤2.0 dB	460HP	FC/F
TW470R1A2 ^{c,d}	0			(Click for Plot)				(Click for Plot)		FC/A
FC488-99B-FC	1	488 nm	±15 nm	99:1		0.7 dB / 21 dB	1.0 dB		460HP	FC/F
FC488-99B-APC	0	400 1111	131111	55.1	-	(Typical)	(Typical)	-	40011	FC/A

Please see the 2x2 Coupler Tutorial tab for more information on these terms.
Other fiber types may be available upon request. Please contact Tech Support with inquiries.

The FC488-99B-FC and FC488-99B-APC will be retired without replacment when stock is depleted. If you require these parts for line production, please contact Tech Support.

 All values are specified at room temperature over the bandwidth and measured without connectors using the white port as the input, as indicated in the state of t

the diagram above; performance may vary if the blue port is used as the input.

Below the cut-off wavelength, single mode operation is not guaranteed (click on the blue info icon for more information).

Part Number	Description	Price	Availability
TW470R1F2	2x2 Wideband Fiber Optic Coupler, 470 ± 40 nm, 99:1 Split, FC/PC	\$398.22	Today
TW470R1A2	2x2 Wideband Fiber Optic Coupler, 470 ± 40 nm, 99:1 Split, FC/APC	\$441.50	Today
FC488-99B-FC	2x2 Fiber Optic Coupler, 488 ± 15 nm, 99:1 Split, FC/PC	\$248.89	Lead Time
FC488-99B-APC	2x2 Fiber Optic Coupler, 488 ± 15 nm, 99:1 Split, FC/APC	\$293.25	Lead Time

Visit the 488 nm Single Mode Fused Fiber Optic Couplers / Taps page for pricing and availability information: https://www.thorlabs.com/newgrouppage9.cfm?objectgroup_id=8438

Specs

Specifications ^a					
Coupling Ratio	90:10				
Center Wavelength	488 nm				
Bandwidth	±15 nm				
Insertion Loss	1.2 dB / 11 dB (Typ.)				
Excess Loss	1.0 dB (Typ.)				
Polarization-Dependent Loss (PDL)	≤0.22 dB				
Directivity	>50 dB				
Fiber Type	460HP				
Port Configuration	2x2				
Fiber Lead Length and Tolerance	0.8 m +0.075 m/-0 m				
Termination	2.0 mm Narrow Key FC/PC				
Package Size	Ø0.16" x 2.36" (Ø4.0 mm x 60.0 mm)				
Jacket	Ø900 µm Loose Furcation Tubing				
Operating Temperature	-40 to 85 °C				